Computer Graphics

- Material Models -

Philipp Slusallek & Arsène Pérard-Gayot

Overview

Last time

- Light: radiance & light sources
- Light transport: rendering equation & formal solutions

• Today

- Reflectance properties:
 - Material models
 - Bidirectional Reflectance Distribution Function (BRDF)
 - Reflection models
- Shading

Next lecture

- Varying (reflection) properties over object surfaces: texturing

REFLECTANCE PROPERTIES

Appearance Samples

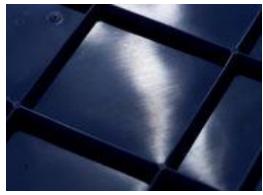
• How do materials reflect light?



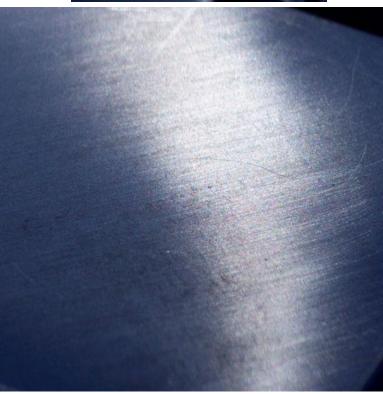
Opaque

Translucency - subsurface scattering

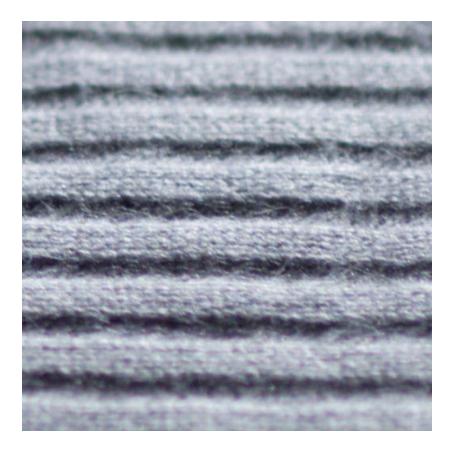
• Anisotropic

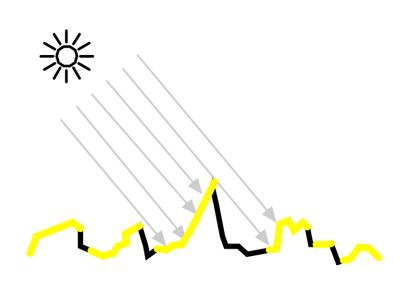






Complex surface meso-structure



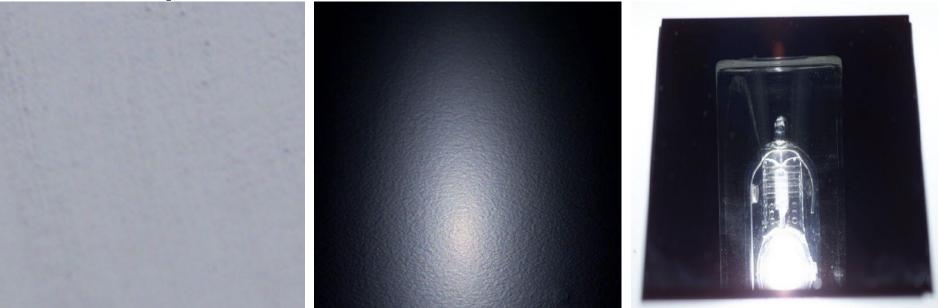


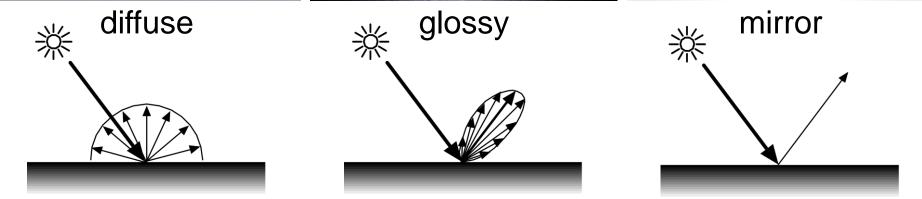
Fibers





 Photos of samples with light source at exactly the same position





How to describe materials?

- Reflection properties
- Mechanical, chemical, electrical properties
- Surface roughness
- Geometry/meso-structure
- Goal: relightable representation of appearance

Reflection Equation - Reflectance

Reflection equation

$$L_o(x,\omega_o) = \int_{\Omega_+} f_r(\omega_i, x, \omega_o) L_i(x, \omega_i) \cos\theta_i d\omega_i$$

- BRDF
 - Ratio of reflected radiance to incident irradiance

$$f_r(\omega_i, x, \omega_o) = \frac{dL_o(x, \omega_o)}{dE_i(x, \omega_i)}$$

BRDF

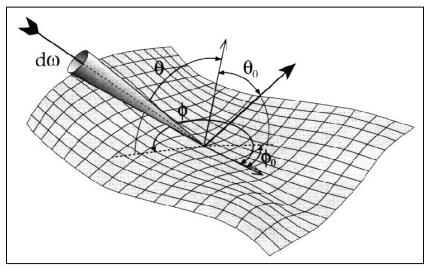
BRDF describes surface reflection

- for light incident from direction $\omega_i = (\theta_i, \varphi_i)$
- observed from direction $\boldsymbol{\omega}_o = (\boldsymbol{\theta}_o, \boldsymbol{\varphi}_o)$

Bidirectional

– Depends on 2 directions ω_i , ω_o and position x (6-D function)

$$f_r(\omega_i, x, \omega_o) = \frac{dL_o(x, \omega_o)}{dE_i(x, \omega_i)} = \frac{dL_o(x, \omega_o)}{L_i(x, \omega_i)\cos\theta_i d\omega_i}$$

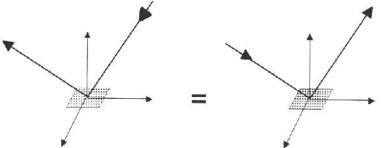


BRDF Properties

Helmholtz reciprocity principle

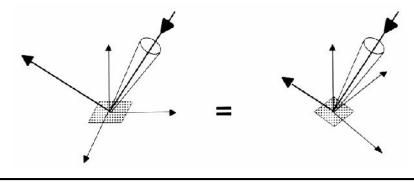
- BRDF remains unchanged if incident and reflected directions are interchanged
- Due to physical law of time reversal

$$f_r(\omega_i, \omega_o) = f_r(\omega_o, \omega_i)$$



- Smooth surface: isotropic BRDF
 - Reflectivity independent of rotation around surface normal
 - BRDF has only 3 instead of 4 directional degrees of freedom

$$f_r(\theta_i, x, \theta_o, \varphi_o - \varphi_i)$$



BRDF Properties

Characteristics

- BRDF units
 - Inverse steradian: sr^{-1} (not intuitive)
- Range of values: distribution function is positive, can be infinite
 - From 0 (total absorption) to ∞ (reflection, δ -function)
- Energy conservation law
 - No self-emission
 - Possible absorption

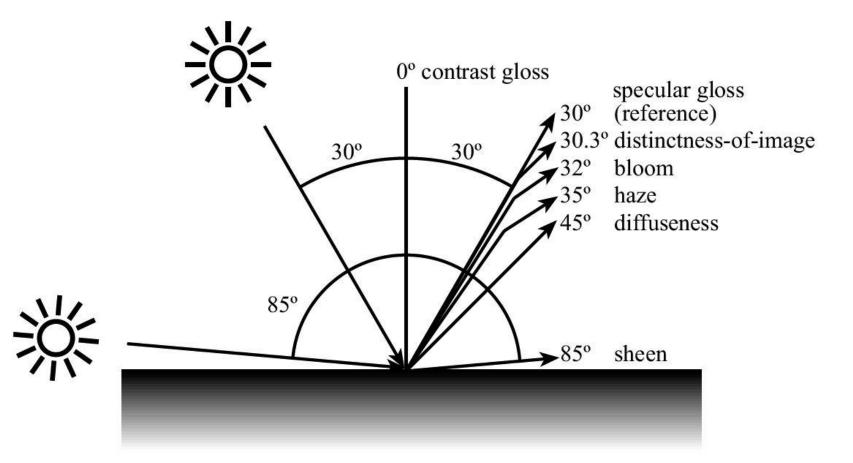
$$\int_{\Omega_{+}} f_{r}(\omega_{i}, x, \omega_{o}) \cos\theta_{o} d\omega_{o} \leq 1, \qquad \forall \omega_{i}$$

• Reflection only at the point of entry $(x_i = x_o)$

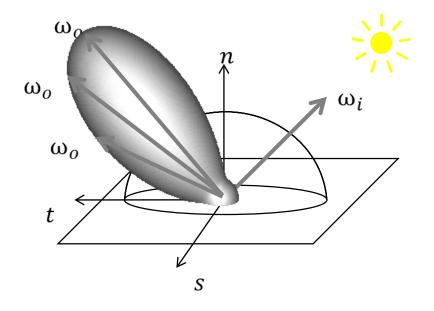
No subsurface scattering

Standardized Gloss Model

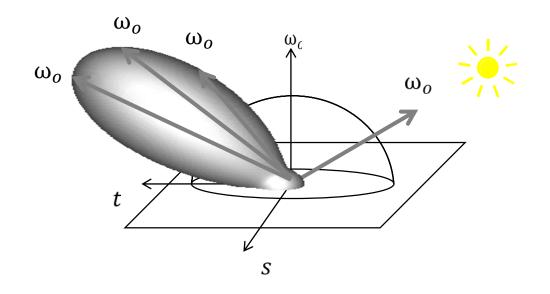
- Industry often uses only a subset of BRDF values
 - Reflection only measured at discrete set of angles



Reflection of an Opaque Surface



Reflection of an Opaque Surface

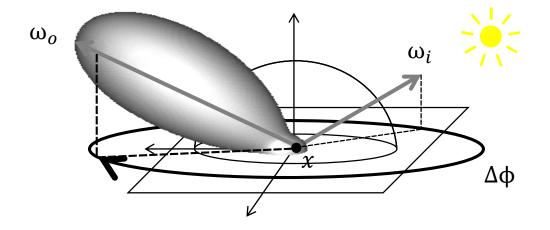


Isotropic BRDF – 3D

Invariant with respect to rotation about the normal

- Only depends on azimuth difference to incoming angle

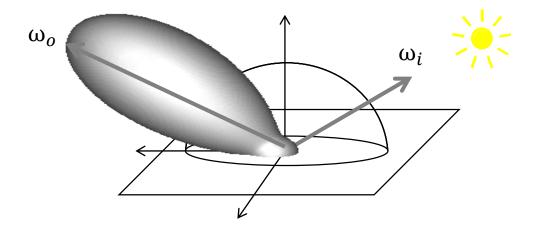
$$f_r((\theta_i, \varphi_i) \to (\theta_o, \varphi_o)) \Longrightarrow$$
$$f_r(\theta_i \to \theta_o, (\varphi_i - \varphi_o)) = f_r(\theta_i \to \theta_o, \Delta \varphi)$$



Homogeneous BRDF – 4D

- Homogeneous bidirectional reflectance
 distribution function
 - Ratio of reflected radiance to incident irradiance

$$f_r(\omega_i \to \omega_o) = \frac{dL_o(\omega_o)}{dE_i(\omega_i)}$$

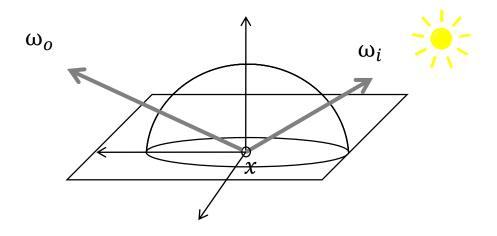


Spatially Varying BRDF – 6D

Heterogeneous materials (standard model for BRDF)

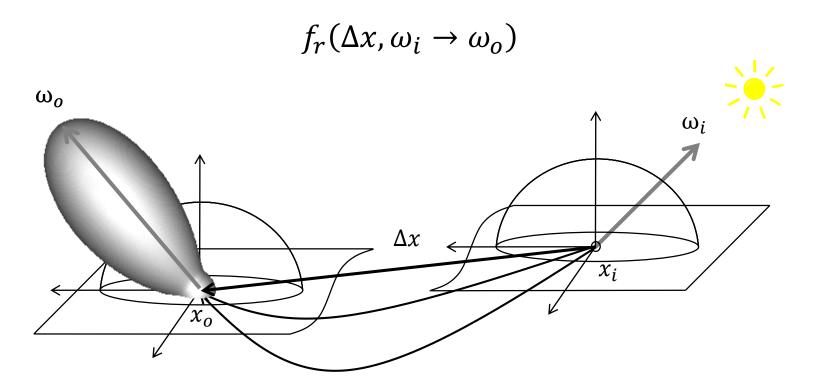
- Dependent on position, and two directions
- Reflection at the point of incidence

$$f_r(x, \omega_i \to \omega_o)$$



Homogeneous BSSRDF – 6D

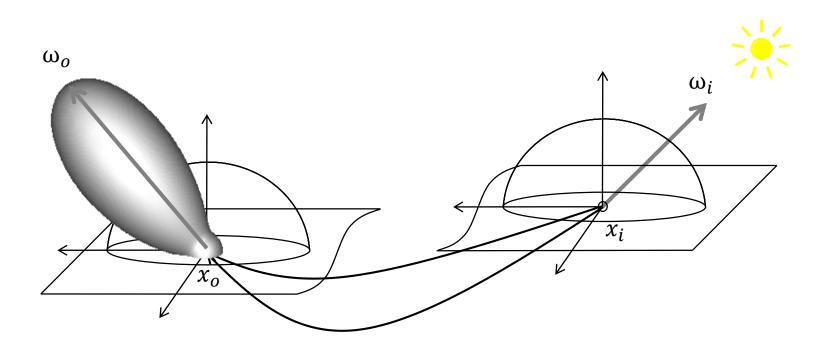
- Homogeneous bidirectional scattering surface reflectance distribution function
 - Assumes a homogeneous and flat surface
 - Only depends on the difference vector to the outgoing point



BSSRDF – 8D

 Bidirectional scattering surface reflectance distribution function

 $f_r((x_i, \omega_i) \to (x_o, \omega_o))$

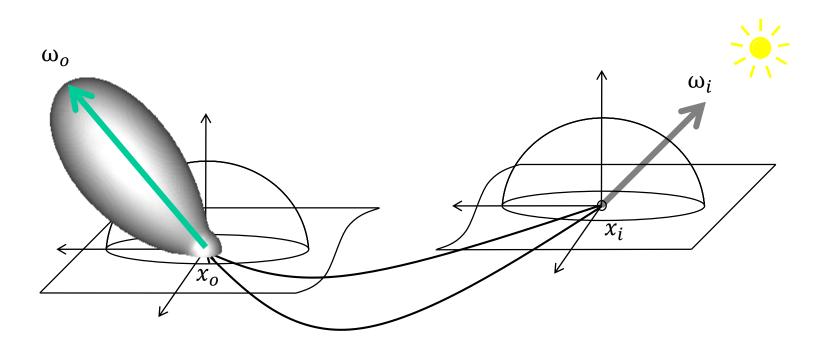


Generalization – 9D

Generalizations

- Add wavelength dependence

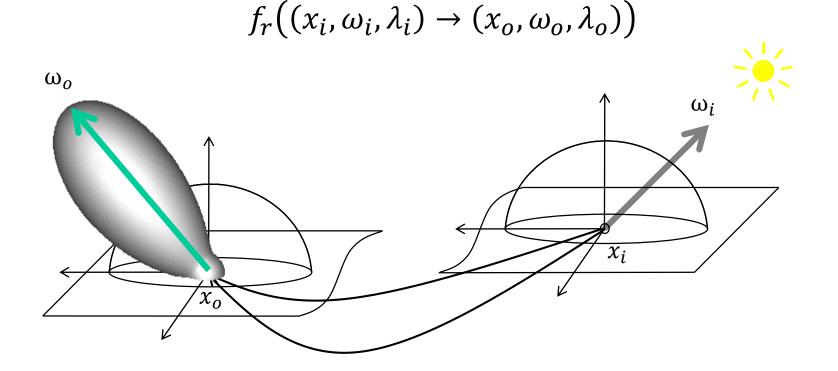
 $f_r(\lambda, (x_i, \omega_i) \to (x_o, \omega_o))$



Generalization – 10D

Generalizations

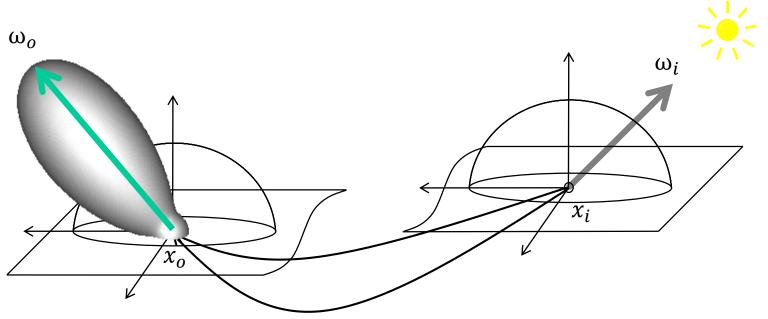
- Add wavelength dependence
- Add fluorescence
 - Change to longer wavelength during scattering



Generalization – 11D

Generalizations

- Add wavelength dependence
- Add fluorescence (change to longer wavelength for reflection)
- Time varying surface characteristics

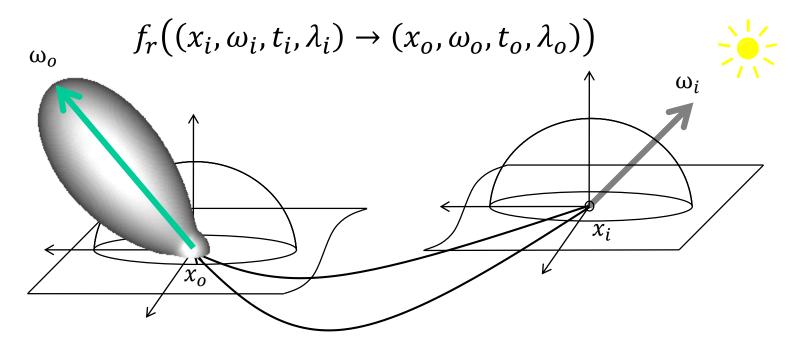


 $f_r(t, (x_i, \omega_i, \lambda_i) \to (x_o, \omega_o, \lambda_o))$

Generalization – 12D

Generalizations

- Add wavelength dependence
- Add fluorescence (change to longer wavelength for reflection)
- Time varying surface characteristics
- Phosphorescence
 - Temporal storage of light



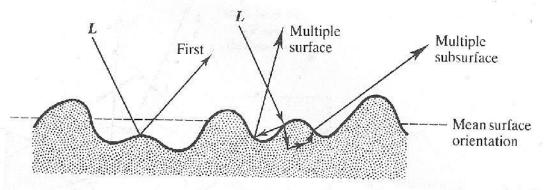
Reflectance

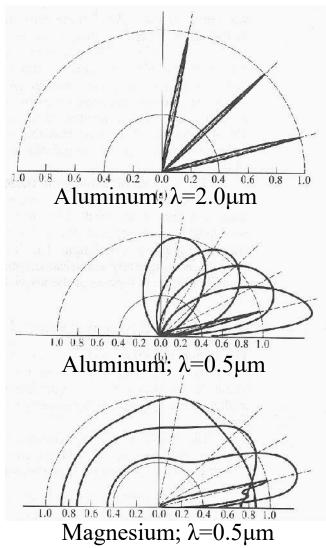
Reflectance may vary with

- Illumination angle
- Viewing angle
- Wavelength
- (Polarization, ...)

Variations due to

- Absorption
- Surface micro-geometry
- Index of refraction / dielectric constant
- Scattering





BRDF Measurement

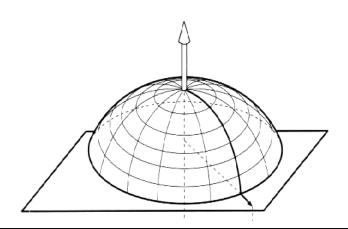
Gonio-Reflectometer

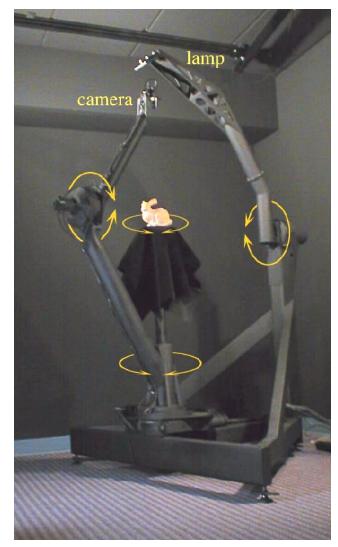
BRDF measurement

- Point light source position (θ_i, φ_i)
- Light detector position (θ_o, φ_o)
- 4 directional degrees of freedom

BRDF representation

- *m* incident direction samples
- n outgoing direction samples
- m*n reflectance values (large!!!)





Stanford light gantry

Rendering from Measured BRDF

- Linearity, superposition principle
 - Complex illumination: integrating light distribution against BRDF
 - Sampled computation: superimposing many point light sources

Interpolation

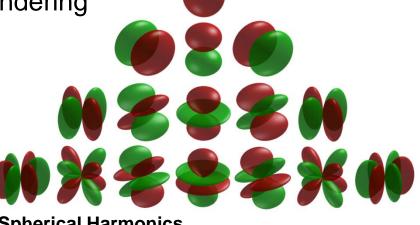
- Look-up of BRDF values during rendering
- Sampled BRDF must be filtered

BRDF Modeling

- Fitting of parameterized BRDF models to measured data
 - Continuous, analytic function
 - No interpolation
 - Typically fast evaluation

Representation in a basis

- Most appropriate: Spherical harmonics
 - Ortho-normal function basis on the sphere
- Mathematically elegant filtering, illumination-BRDF integration



Spherical Harmonics Red is positive, green negative [Wikipedia]

BRDF Modeling

Phenomenological approach

- Description of visual surface appearance
- Composition of different terms:

Ideal diffuse reflection

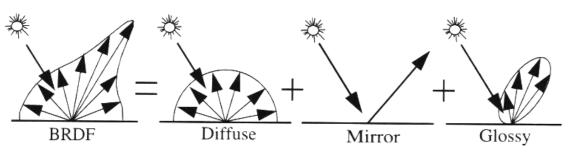
- Lambert's law, interactions within material
- Matte surfaces

Ideal specular reflection

- Reflection law, reflection on a planar surface
- Mirror

Glossy reflection

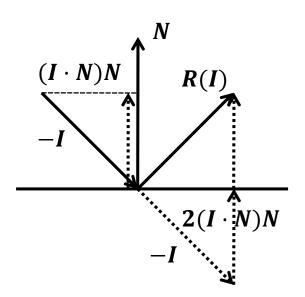
- Directional diffuse, reflection on surface that is somewhat rough
- Shiny surface
- Glossy highlights



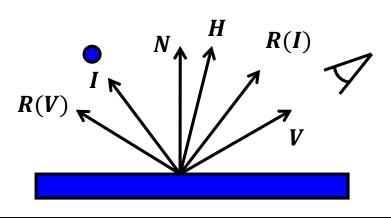
Reflection Geometry

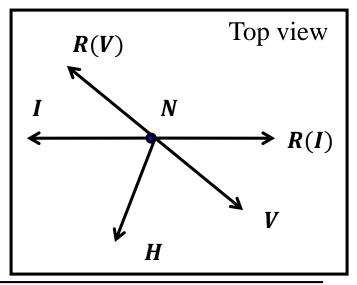
• Direction vectors (normalize):

- N: Surface normal
- *I*: Light source direction vector
- V: Viewpoint direction vector
- R(I): Reflection vector
 - $R(I) = -I + 2(I \cdot N)N$
- H: Halfway vector
 - H = (I + V) / |I + V|



Tangential surface: local plane

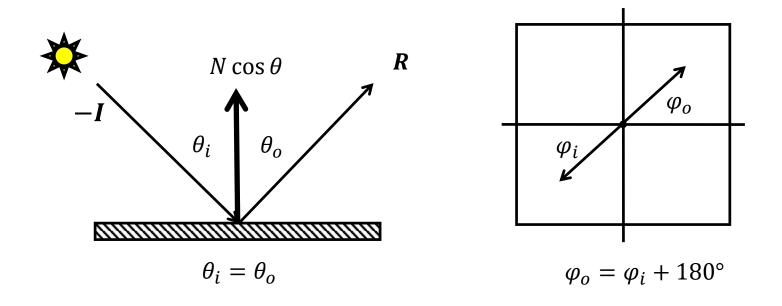




Ideal Specular Reflection

- Angle of reflectance equal to angle of incidence
- Reflected vector in a plane with incident ray and surface normal vector

$$R + I = 2 \cos \theta N = 2(I \cdot N)N \Longrightarrow$$
$$R(I) = -I + 2(I \cdot N)N$$



Mirror BRDF

• Dirac Delta function $\delta(x)$

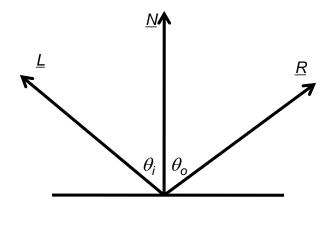
- $\delta(x)$: zero everywhere except at x = 0
- Unit integral iff domain contains x = 0 (else zero)

$$f_{r,m}(\omega_i, x, \omega_o) = \rho_s(\theta_i) \frac{\delta(\cos\theta_i - \cos\theta_o)}{\cos\theta_i} \delta(\varphi_i - \varphi_o \pm \pi)$$
$$L_o(x, \omega_o) = \int_{\Omega_+} f_{r,m}(\omega_i, x, \omega_o) L_i(x, \omega_i) \cos\theta_i d\omega_i = \rho_s(\theta_o) L_i(x, \theta_o, \varphi_o \pm \pi)$$

• Specular reflectance ρ_s

- Ratio of reflected radiance in specular direction and incoming radiance
- Dimensionless quantity between 0 and 1

$$\rho_s(x,\theta_i) = \frac{L_o(x,\theta_o)}{L_i(x,\theta_o)}$$



Refraction in Dielectrics

• Time required for light to travel from A to B through C

$$t_{AB} = t_{AC} + t_{CB} = \frac{\|AC\|}{c_a} + \frac{\|BC\|}{c_b} = \frac{\sqrt{(C_x - A_x)^2 + A_y^2}}{c_a} + \frac{\sqrt{(C_x - B_x)^2 + B_y^2}}{c_b}$$
(assuming $C_y = 0$)

Fermat's principle: light path of least traversal time

$$\frac{dt_{AB}}{dC_x} = \frac{C_x - A_x}{c_a \sqrt{(C_x - A_x)^2 + A_y^2}} + \frac{C_x - B_x}{c_b \sqrt{(C_x - B_x)^2 + B_y^2}} = \frac{C_x - A_x}{c_a \|AC\|} + \frac{C_x - B_x}{c_b \|BC\|}$$

$$= \frac{sin(\theta_a)}{c_a} + \frac{-sin(\theta_b)}{c_b} = \frac{n_a sin(\theta_a)}{c_0} - \frac{n_b sin(\theta_b)}{c_0} = 0$$

$$= 0$$
plane of incidence
$$\int A_x - B_x + \frac{n_a sin(\theta_a)}{c_b} = \frac{n_a sin(\theta_a)}{c_0} - \frac{n_b sin(\theta_b)}{c_0} = 0$$

- Snell's law: $n_a sin(\theta_a) = n_b sin(\theta_b)$
- Special case possible when $\eta_b < \eta_a$

$$i A n r n_{a} (= n_{i})$$

$$\theta_{1}\theta_{1}C \eta_{1}$$
boundary
$$\theta_{2}$$

$$t B \eta_{2}$$

$$n_{b} (= n_{t})$$

 $\theta_2 = \pi/2$

ηı

 η_2

- If
$$sin(\theta_a) > n_b/n_a$$
 then $n_b = n_a \frac{n_b}{n_a} < n_a sin(\theta_a) = n_b sin(\theta_b)$

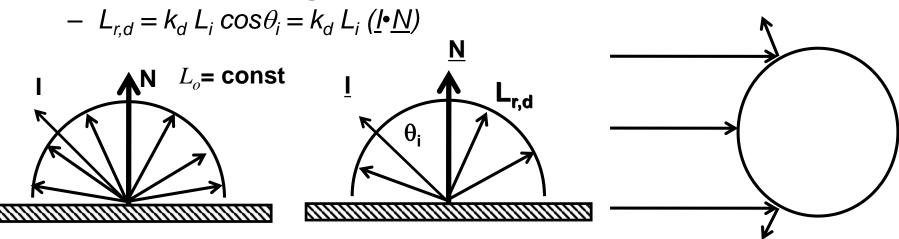
− Which is impossible since $sin(θ_b) \le 1$ ⇒ total internal reflection

Lambertian Diffuse Reflection

- Light equally likely to be reflected in any output direction (independent of input direction)
- Constant BRDF

 $f_{r,d}(\omega_i, x, \omega_o) = k_d = const$ $L_o(x, \omega_o) = k_d \int_{\Omega_+} L_i(x, \omega_i) \cos \theta_i \, d\omega_i = k_d E$

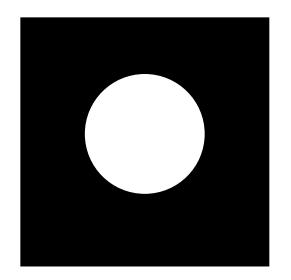
- k_d : diffuse coefficient, material property [1/sr]
- For each point light source



Lambertian Objects

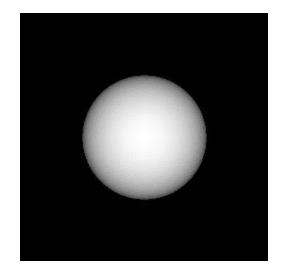
Self-Iuminous spherical Lambertian light source

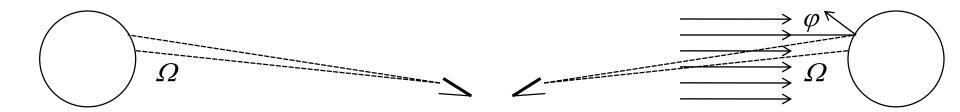
 $\Phi_0 \propto L_0 \cdot \Omega$



Eye-light illuminated spherical Lambertian reflector

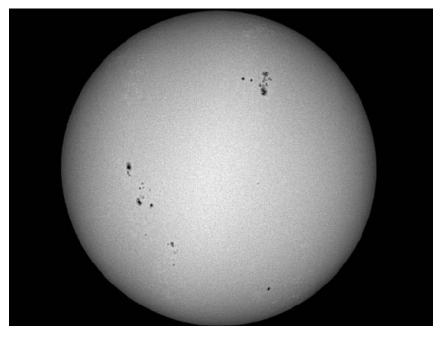
 $\Phi_1 \propto L_{\rm i} \cdot \cos \theta \cdot \Omega$





Lambertian Objects (?)

The Sun



- Some absorption in photosphere
- Path length through photosphere longer from the Sun's rim

The Moon



- Surface covered with fine dust
- Dust visible best from slanted viewing angle

 \Rightarrow Neither the Sun nor the Moon are Lambertian

"Diffuse" Reflection

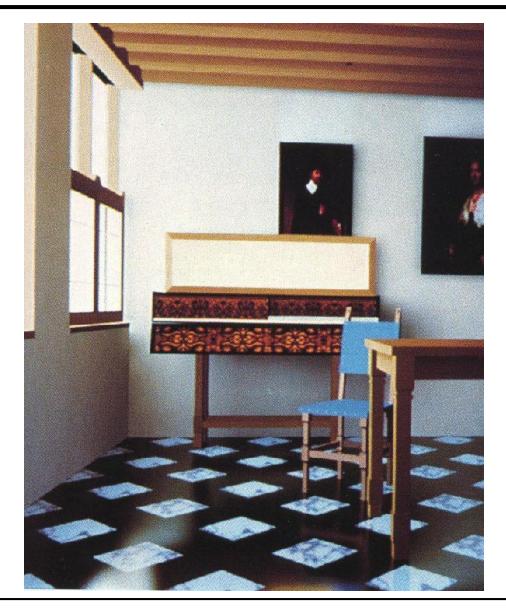
Theoretical explanation

- Multiple scattering with in the material (at very short range)

Experimental realization

- Pressed magnesium oxide powder
 - Random mixture of tiny, highly reflective particles
- Almost never valid at grazing angles of incidence
- Paint manufacturers attempt to create ideal diffuse paints

Glossy Reflection

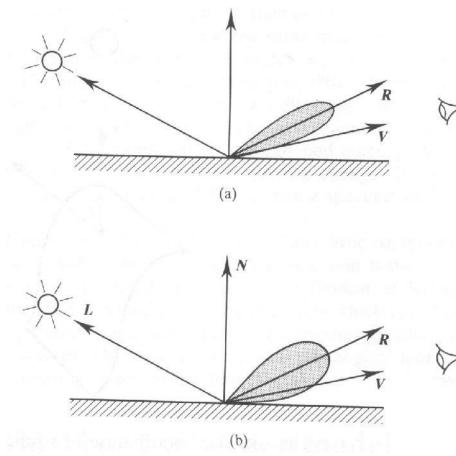


Glossy Reflection

- Due to surface roughness
- Empirical models (phenomenological)
 - Phong
 - Blinn-Phong

Physically-based models

- Blinn
- Cook & Torrance



Phong Glossy Reflection Model

• Simple description: Cosine power lobe

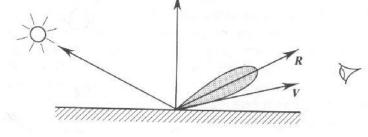
 $f_r(\omega_i, x, \omega_o) = k_s (R(I) \cdot V)^{k_e} / I \cdot N$

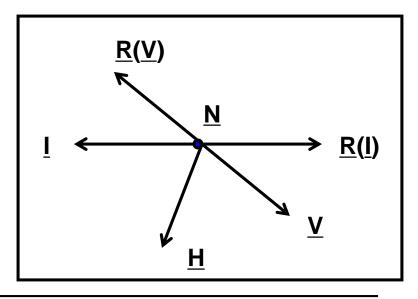
- Take angle to reflection direction to some $- L_{r,s} = L_i k_s \cos^{ke} \theta_{RV}$
- Issues
 - Not energy conserving/reciprocal
 - Plastic-like appearance

Dot product & power

- Still widely used in CG

$$\overset{\theta(HN)}{\underline{H}} \overset{\underline{R}(\underline{I})}{\underline{I}}$$

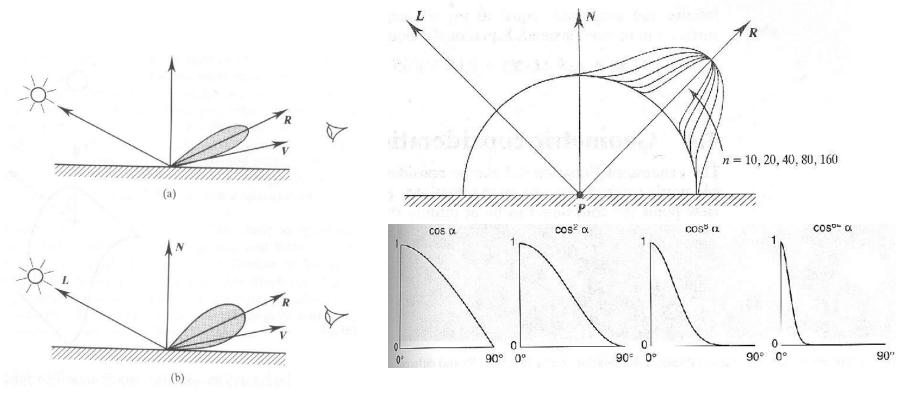




Phong Exponent k_e

 $f_r(\omega_i, x, \omega_o) = k_s (R(I) \cdot V)^{k_e} / I \cdot N$

• Determines size of highlight



Beware: Non-zero contribution into the material !!!

Blinn-Phong Glossy Reflection

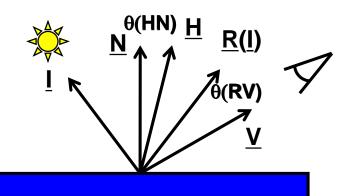
Same idea: Cosine power lobe

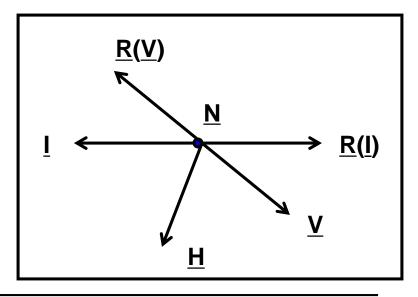
 $f_r(\omega_i, x, \omega_o) = k_s (H \cdot N)^{k_e} / I \cdot N$

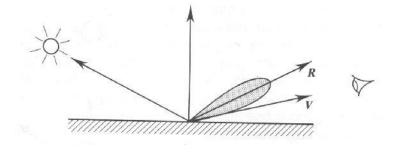
- $L_{r,s} = L_i k_s \cos^{ke} \Theta_{HN}$
- Dot product & power
 - $\Theta_{RV} \rightarrow \Theta_{HN}$

- Special case: Light source, viewer far away

- *I*, *R* constant: *H* constant
- $\boldsymbol{\Theta}_{HN}$ less expensive to compute

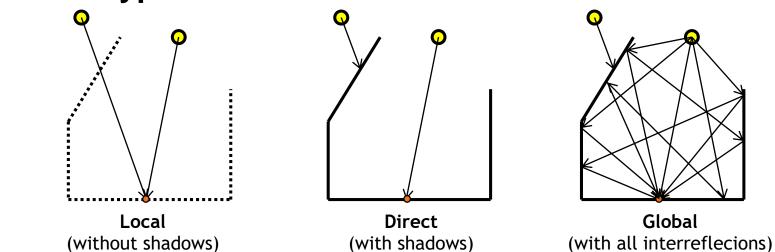






Different Types of Illumination

Three types of illumination



Ambient Illumination

- Global illumination is costly to compute
- Indirect illumination (through interreflections) is typically smooth
- \rightarrow Approximate via a constant term $L_{i,a}$ (incoming ambient illum)
- Has no incoming direction, provide ambient reflection term k_a

$$L_o(x, \omega_o) = k_a L_{i,a}$$

Full Phong Illumination Model

• Phong illumination model for *multiple* point light sources

$$L_r = k_a L_{i,a} + k_d \sum_l L_l(I_l \cdot N) + k_s \sum_l L_l(R(I_l) \cdot V)^{k_e} (Phong)$$
$$L_r = k_a L_{i,a} + k_d \sum_l L_l(I_l \cdot N) + k_s \sum_l L_l(H_l \cdot N)^{k_e} (Blinn)$$

- Diffuse reflection (contribution only depends on incoming cosine)
- Ambient and Glossy reflection (Phong or Blinn-Phong)
- Typically: Color of specular reflection k_s is white
 - Often separate specular and diffuse color (common extension, OGL)

Empirical model!

- Contradicts physics
- Purely local illumination
 - Only direct light from the light sources, constant ambient term
- Optimization: Lights & viewer assumed to be far away

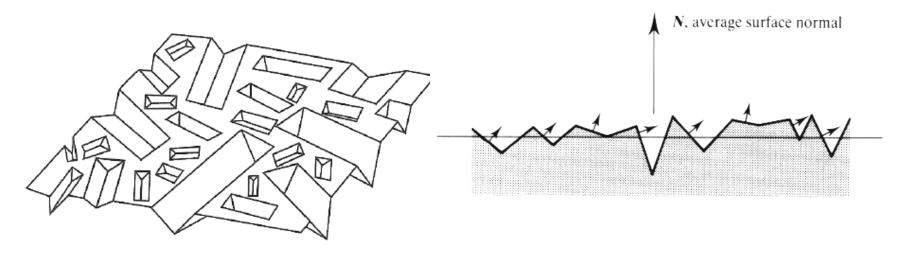
Microfacet BRDF Model

Physically-Inspired Models

- Isotropic microfacet collection
- Microfacets assumed as perfectly smooth reflectors

• BRDF

- Distribution of microfacets
 - Often probabilistic distribution of orientation or V-groove assumption
- Planar reflection properties
- Self-masking, shadowing



Ward Reflection Model

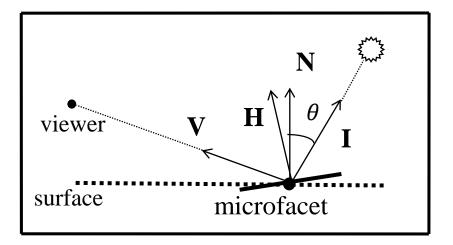
• BRDF

$$f_r = \frac{\rho_d}{\pi} + \frac{\rho_s}{\sqrt{(I \cdot N)(V \cdot N)}} \frac{\exp\left(-\frac{tan^2 \angle H, N}{\sigma^2}\right)}{4\pi\sigma^2}$$

- $-\sigma$ standard deviation (RMS) of surface slope
- Simple expansion to anisotropic model (σ_x , σ_y)
- Empirical, not physics-based

Inspired by notion of reflecting microfacets

- Convincing results
- Good match to measured data



Cook-Torrance Reflection Model

Cook-Torrance reflectance model

- Is based on the *microfacet* model
- BRDF is defined as the sum of a diffuse and a specular component:

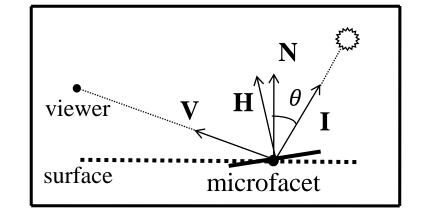
$$f_r = \kappa_d \rho_d + \kappa_s \rho_s; \quad \rho_d + \rho_s \le 1$$

where ρ_s and ρ_d are the specular and diffuse coefficients.

– Derivation of the specular component κ_s is based on a physically derived theoretical reflectance model

Cook-Torrance Specular Term

$$\kappa_s = \frac{F_{\lambda} DG}{\pi (N \cdot V)(N \cdot I)}$$



• D : Distribution function of microfacet orientations

G : Geometrical attenuation factor

- represents self-masking and shadowing effects of microfacets

• F_{λ} : Fresnel term

- computed by Fresnel equation
- Fraction of specularly reflected light for each planar microfacet
- N-V : Proportional to visible surface area
- N-I : Proportional to illuminated surface area

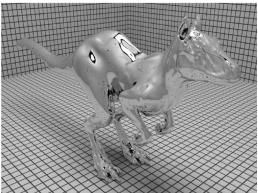
Electric Conductors (e.g. Metals)

- Assume ideally smooth surface
- Perfect specular reflection of light, rest is absorbed
- Reflectance is defined by Fresnel formula based on:
 - Index of refraction η
 - Absorption coefficient $\boldsymbol{\kappa}$
 - Both wavelength dependent

Object	η	k
Gold	0.370	2.820
Silver	0.177	3.638
Copper	0.617	2.63
Steel	2.485	3.433

Given for parallel and perpendicular polarized light

$$r_{\parallel}^{2} = \frac{(\eta^{2} + k^{2})\cos\theta_{i}^{2} - 2\eta\cos\theta_{i} + 1}{(\eta^{2} + k^{2})\cos\theta_{i}^{2} + 2\eta\cos\theta_{i} + 1}$$
$$r_{\perp}^{2} = \frac{(\eta^{2} + k^{2}) - 2\eta\cos\theta_{i} + \cos\theta_{i}^{2}}{(\eta^{2} + k^{2}) + 2\eta\cos\theta_{i} + \cos\theta_{i}^{2}}.$$



 $- \theta_i$, θ_t : Angle between ray & plane, incident & transmitted

For unpolarized light:

$$F_{\rm r} = \frac{1}{2}(r_{\parallel}^2 + r_{\perp}^2)$$

Dielectrics (e.g. Glass)

- Assume ideally smooth surface
- Non-reflected light is perfectly transmitted: 1 F_r
 - They do not conduct electricity
- Fresnel formula depends on:
 - Refr. index: speed of light in vacuum vs. medium
 - Refractive index in incident medium $\eta_i = c_0 / c_i$
 - Refractive index in transmitted medium $\eta_t = c_0 / c_t$

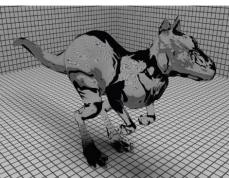
Given for parallel and perpendicular polarized light

$$r_{\parallel} = \frac{\eta_{t} \cos \theta_{i} - \eta_{i} \cos \theta_{t}}{\eta_{t} \cos \theta_{i} + \eta_{i} \cos \theta_{t}}$$
$$r_{\perp} = \frac{\eta_{i} \cos \theta_{i} - \eta_{t} \cos \theta_{t}}{\eta_{i} \cos \theta_{i} + \eta_{t} \cos \theta_{t}},$$

For unpolarized light:

Medium	Index of refraction η	
Vacuum	1.0	
Air at sea level	1.00029	
Ice	1.31	
Water (20° C)	1.333	
Fused quartz	1.46	
Glass	1.5–1.6	
Sapphire	1.77	
Diamond	2.42	

$$F_{\rm r} = \frac{1}{2}(r_{\parallel}^2 + r_{\perp}^2)$$



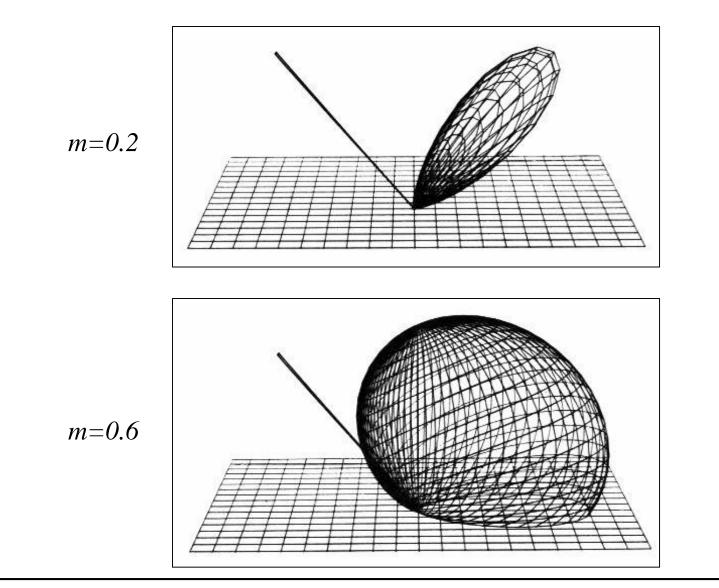
Microfacet Distribution Functions

- Isotropic Distributions $D(\omega) \Rightarrow D(\alpha) \quad \alpha = \angle N, H$
 - $-\alpha$: angle to average normal of surface
 - -m: average slope of the microfacets
- Blinn:
- Torrance-Sparrow
 - Gaussian

$$D(\alpha) = \cos^{-\frac{\ln 2}{\ln \cos m}}(\alpha)$$
$$D(\alpha) = e^{-\ln 2\left(\frac{\alpha}{m}\right)^2}$$

- Beckmann $D(\alpha) = \frac{1}{\pi m^2 \cos^4 \alpha} e^{-(\frac{\tan \alpha}{m})^2}$
 - Used by Cook-Torrance

Beckman Microfacet Distribution



Geometric Attenuation Factor

- V-shaped grooves
- Fully illuminated and visible

G = 1

• Partial masking of reflected light

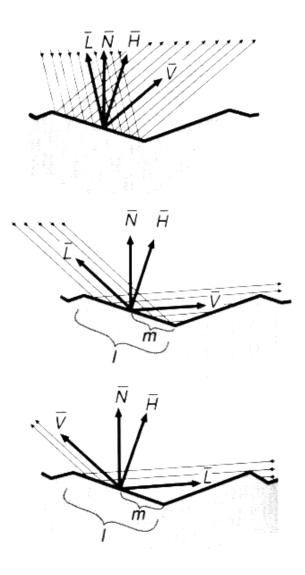
 $G = \frac{2(\underline{N} \cdot \underline{H})(\underline{N} \cdot \underline{V})}{(\underline{V} \cdot \underline{H})}$

Partial shadowing of incident light

$$G = \frac{2(\underline{N} \cdot \underline{H})(\underline{N} \cdot \underline{I})}{(\underline{V} \cdot \underline{H})}$$

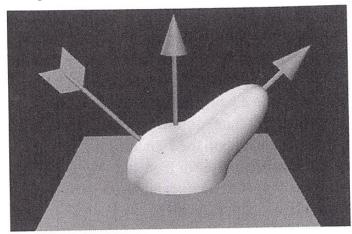
• Final

$$G = min\left\{1, \frac{2(\underline{N} \cdot \underline{H})(\underline{N} \cdot \underline{V})}{(\underline{V} \cdot \underline{H})}, \frac{2(\underline{N} \cdot \underline{H})(\underline{N} \cdot \underline{I})}{(\underline{V} \cdot \underline{H})}\right\}$$



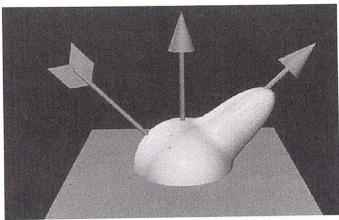
Comparison Phong vs. Torrance

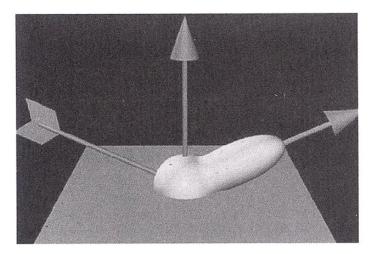
Phong:



(a)

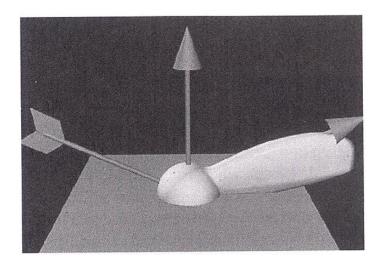
Torrance:





(b)

(d)



SHADING

What is necessary?

- View point position
- Light source description
- Reflectance model
- Surface normal / local coordinate frame

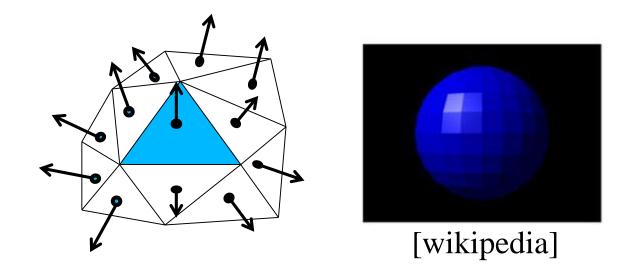
Surface Normals – Triangle Mesh

Most simple: Constant Shading

- Fixed color per polygon/triangle

Shading Model: Flat Shading

- Single per-surface normal
- Single color per polygon
- Evaluated at one of the vertices (\rightarrow OGL) or at center



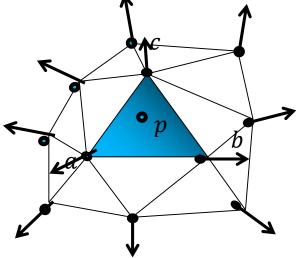
Surface Normals – Triangle Mesh

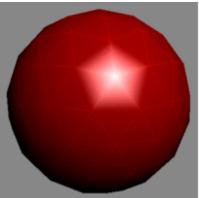
Shading Model: Gouraud shading

- Per-vertex normal
 - Can be computed from adjacent triangle normals (e.g. by averaging)
- Linear interpolation of the shaded colors
 - · Computed at all vertices and interpolated
- Often results in shading artifacts along edges
 - Mach Banding (i.e. discontinuous 1st derivative)
 - Flickering of highlights (when one of the normal generates strong reflection)

 $L_x \sim f_r(\omega_o, n_x, \omega_i) L_i \cos \theta_i$ $L_p = \lambda_1 L_a + \lambda_2 L_b + \lambda_3 L_c$

 Barycentric interpolation within triangle



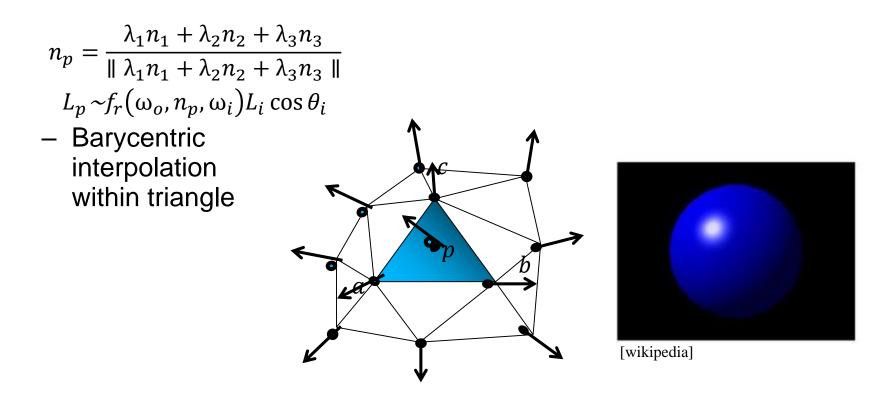


[wikipedia]

Surface Normals – Triangle Mesh

Shading Model: Phong shading

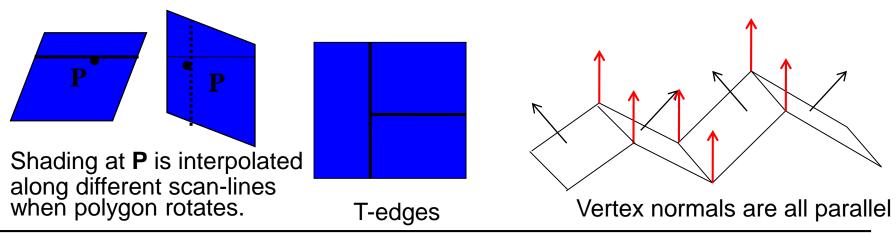
- Linear interpolation of the surface normal
- Shading is evaluated at every point separately
- Smoother but still off due to hit point offset from apparent surface



Problems in Interpolated Shading

Issues

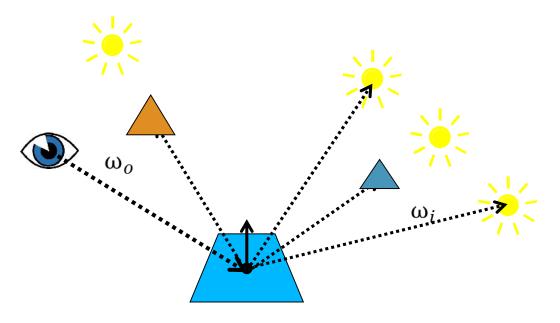
- Polygonal silhouette may not match the smooth shading
- Perspective distortion
 - Interpolation in 2-D screen space rather than world space (==> later)
- Orientation dependence
 - Only for polygons
 - Not with triangles (here linear interpolation is rotation-invariant)
- Shading discontinuities at shared vertices (T-edges)
- Unrepresentative normal vectors



Occlusions

The point on the surface might be in shadow

- Rasterization (OpenGL):
 - Not easily done
 - Can use shadow map or shadow volumes (→ later)
- Ray tracing
 - Simply trace ray to light source and test for occlusion



Area Light sources

Typically approximated by sampling

- Replacing it with some point light sources
 - Often randomly sampled
 - Cosine distribution of power over angular directions

